

Forced convective heat transfer in a porous medium

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Abstract

This paper deals with a steady flow of a viscous fluid of finite depth in a porous medium over a fixed horizontal, impermeable bottom. Exact solutions of Momentum and Energy equations are obtained when the temperatures on the fixed bottom and on the free surface are prescribed. Flow rate, Mean velocity, Temperature, Mean Temperature in the flow region and the Nusselt number on the boundaries have been obtained. The cases of small depth (shallow fluid) and large depth (deep fluid) are also discussed. The results are illustrated graphically.

Keywords: Velocity, Mean Velocity, Temperature, Mean Temperature, Porosity

Introduction:

Forced convective flows through porous and non porous channels of a variety of geometries was examined by Raghavacharyulu [1] in 1984. Jaweed Ameen [2] studied some investigations on fluid flows through generalized porous media. Ph.D Thesis (2009) Banasthali University. M.K. Alkam et al [3] studied heat transfer in parallel-plate channels by using porous inserts. In the year 2003 A. Haji-sheikh & K.Vafai [4] worked on the analysis of flow and heat transfer in porous media imbedded inside various-shaped ducts. H.A.Attia et al [5] studied an unsteady flow in a porous medium between parallel plates in the presence of uniform suction and injection with heat transfer. K.V.S. Raju et al [6] studied the convective flow through porous medium in a horizontal channel with insulated impermeable bottom in the presence of magnetic field, viscous dissipation and Joule heating.

In this paper the steady forced convective flow of a viscous liquid of viscosity μ and of finite depth H through a porous medium of porosity coefficient ' k^* ' over a fixed impermeable bottom is investigated.

The flow is generated by a constant pressure gradient parallel to the fixed bottom plate. The momentum equation considered is the generalized Darcy's law proposed by Yama Moto and Iwamura[7] which takes into account the convective acceleration and the Newtonian viscous stresses in addition to the classical Darcy force.

The basic equations of momentum and energy are solved to give exact expressions for velocity and temperature distributions. Employing the flow rate, mean velocity, mean temperature, mean mixed temperature and the nusselt numbers at the fluid boundaries have been obtained and illustrated graphically.

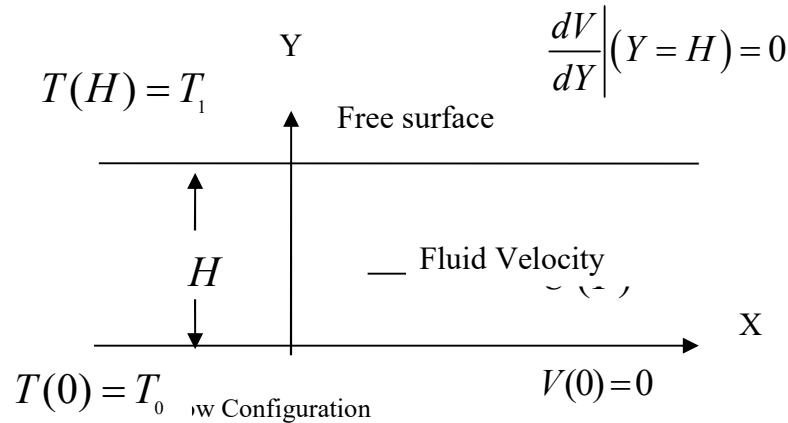
The cases of 1. Shallow depths (small H) and 2. Large depths (large H) are also discussed.

Mathematical Formulation

In the formulation of the problem let us consider the steady forced convective flow of a viscous fluid through a porous medium of viscosity coefficient μ and of finite depth (H) over a fixed horizontal impermeable bottom. The

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flow is generated by a constant horizontal pressure gradient parallel to the bottom. Further the bottom is kept at a constant temperature T_0 and the free surface is exposed to atmospheric temperature T_1 .



With reference to a rectangular Cartesian co-ordinates system with the origin 'O' on the bottom, X-axis in the flow direction (that is parallel to the applied pressure gradient). The Y-axis vertically upwards, the bottom is represented as $Y=0$ and the free surface as $Y=H$. Let the flow be characterized by a velocity $V = (V(Y), 0, 0)$. This choice of velocity evidently satisfies the continuity equation $\nabla \cdot V = 0$ where V is the fluid velocity vector. Further let $T(Y)$ denotes the temperature distribution.

Basic Equations:

Let the convective flow be calculated by the velocity field $V = (V(Y), 0, 0)$ and the temperature $T(Y)$. This

choice of the velocity satisfies the continuity equation $\nabla \cdot V = 0$ (1)

The Momentum Equation is

$$-\frac{\partial P}{\partial X} + \mu \frac{d^2 V}{dY^2} - \mu \frac{V}{k^*} = 0 \quad (2)$$

and the Energy Equation is

$$\rho c V \frac{\partial T}{\partial X} = K \frac{d^2 T}{dY^2} + \mu \left(\frac{dV}{dY} \right)^2 \quad (3)$$

In the above equations ρ is the fluid density, k^* the coefficient of porosity of the medium, c is the specific heat, K the thermal conductivity of the fluid and P the fluid pressure.

Boundary Conditions:

Since the bottom is fixed,

$$V(0) = 0 \quad (4)$$

At the free surface shear stress vanishes

$$\mu \frac{dV}{dY} = 0 \text{ at } Y=H. \quad (5)$$

$$\text{Also } T(0) = T_0 \quad \text{-----(6)} \quad \text{and} \quad T(H) = T_1 \quad (7)$$

where T_0 is the bottom temperature and T_1 is the atmosphere temperature.

In terms of the non-dimensional variables defined as:

$$Y=ay; \quad X=ax; \quad H=ah; \quad V = \frac{\mu v}{\rho a^2}; \quad P = \frac{\mu^2 p}{\rho a^2}; \quad T = T_0 + (T_1 - T_0)\theta; \quad \text{Pr} = \frac{\mu c}{k}; \quad k^* = \frac{a^2}{\alpha^2};$$

$$E = \frac{\mu^3}{\rho^2 a^2 K (T_1 - T_0)}; \quad -\frac{\partial P}{\partial X} = \frac{\mu^2 c_1}{\rho a^3} \left(c_1 = -\frac{\partial p}{\partial x} \right) \quad \text{and} \quad \frac{\partial T}{\partial X} = \frac{(T_1 - T_0)}{a} c_2 \quad \text{where} \quad c_2 = \frac{\partial \theta}{\partial x}$$

(8)

where 'a' is some standard length, the basic field equations (2), (3) can be rewritten as follows:

Momentum Equation:

$$\frac{d^2 v}{dy^2} - \alpha^2 v = -c_1 \quad (9) \quad \text{and}$$

Energy Equation:

$$\frac{d^2 \theta}{dy^2} = \text{Pr} c_2 v - E \left(\frac{dv}{dy} \right)^2 \quad (10)$$

together with the boundary conditions

$$\text{For the velocity } v(0) = 0 \text{ and } \frac{dv}{dy} = 0 \text{ at } y=h \quad (11)$$

$$\text{and for the temperature } \theta(0) = 0 \text{ and } \theta(h) = 1 \quad (12)$$

The momentum equation together with the related boundary conditions yield the velocity distribution:

$$v(y) = \frac{c_1}{\alpha^2} \left(1 - \frac{\cosh \alpha(h-y)}{\cosh \alpha h} \right) \quad (13)$$

The energy equation satisfying the boundary conditions yields the temperature distribution:

$$\theta(y) = \frac{y}{h} + \frac{Pr c_1 c_2}{\alpha^2} \left[\frac{(h-y)}{h \alpha^2} - \frac{y(h-y)}{2} + \frac{1}{\alpha^2 \cosh \alpha h} \left(\frac{y}{h} - \cosh \alpha(h-y) \right) \right] +$$

$$\frac{Ec_1^2}{2 \alpha^2 \cosh^2 \alpha h} \left[\frac{(h-y) \cosh(2 \alpha h)}{4 \alpha^2 h} - \frac{y(h-y)}{2} + \frac{1}{4 \alpha^2} \left(\frac{y}{h} - \cosh 2 \alpha(h-y) \right) \right]$$

(14)

The flow rate in the non-dimensional form is

$$q = \int_0^h v(y) dy = \frac{c_1}{\alpha^2} \left(h - \frac{\tanh \alpha h}{\alpha} \right)$$

The mean velocity in the non-dimensional form is

$$\frac{1}{h} \int_0^h v(y) dy = \frac{c_1}{h \alpha^2} \left(h - \frac{\tanh \alpha h}{\alpha} \right) \quad (15)$$

Further the mean temperature in non-dimensional form is given by

$$\bar{\theta} = \frac{1}{h} \int_0^h \theta dy$$

$$= \frac{1}{2} + \frac{Pr c_1 c_2}{\alpha^2} \left(\frac{-h^2}{12} + \frac{1}{2 \alpha^2} + \frac{1}{2 \alpha^2 \cosh \alpha h} - \frac{\tanh \alpha h}{h \alpha^3} \right) -$$

$$\frac{Ec_1^2}{2 \alpha^2 \cosh^2 \alpha h} \left(\frac{-1}{8 \alpha^2} + \frac{h^2}{12} - \frac{\cosh 2 \alpha h}{8 \alpha^2} + \frac{\sinh 2 \alpha h}{8 h \alpha^3} \right)$$

(16)

Heat transfer rate (Nusselt Number):

On the bottom:

$$\frac{d\theta}{dy} \Big|_{y=0} = \frac{1}{h} + \frac{Pr c_1 c_2}{\alpha^2} \left(\frac{\tanh \alpha h}{\alpha} - \frac{h}{2} + \frac{1}{h \alpha^2 \cosh \alpha h} - \frac{1}{h \alpha^2} \right) -$$

$$\frac{Ec_1^2}{2 \alpha^2 \cosh^2 \alpha h} \left(\frac{\sinh 2 \alpha h}{-2 \alpha} - \frac{1}{4 h \alpha^2} + \frac{h}{2} + \frac{\cosh 2 \alpha h}{4 h \alpha^2} \right)$$

(17)

On the free surface :

$$\frac{d\theta}{dy} \Big|_{y=h} = \frac{1}{h} + \frac{Pr c_1 c_2}{\alpha^2} \left(\frac{h}{2} + \frac{1}{h \alpha^2 \cosh \alpha h} - \frac{1}{h \alpha^2} \right) - \frac{Ec_1^2}{2 \alpha^2 \cosh^2 \alpha h} \left(-\frac{h}{2} - \frac{1}{4 h \alpha^2} + \frac{\cosh 2 \alpha h}{4 h \alpha^2} \right) \quad (18)$$

1. Flow for large depths that is for large H:

For large h $\sinh \alpha h \approx \frac{e^{\alpha h}}{2}$; $\cosh \alpha h \approx \frac{e^{\alpha h}}{2}$; $\tanh \alpha h \approx 1$ and neglecting terms of $O(\frac{1}{h^3})$.

$$\text{Velocity: } v(y) = \frac{c_1}{\alpha^2} (1 - e^{-\alpha y}) \quad (19)$$

Mean velocity:

$$v(y) = \frac{c_1}{h \alpha^2} \left(h - \frac{1}{\alpha} \right) \quad (20)$$

Temperature:

$$\theta = \frac{y}{h} + \frac{Pr c_1 c_2}{\alpha^2} \left[\frac{1}{h \alpha^2} (h - y) - \frac{y}{2} (h - y) - \frac{e^{-\alpha y}}{\alpha^2} \right] + \frac{Ec_1^2}{\alpha^2} \left[\frac{h - y}{4 \alpha^2 h} - \frac{e^{-2 \alpha y}}{4 \alpha^2} \right] \quad (21)$$

Mean temperature

$$\bar{\theta} = \frac{1}{2} + \frac{Pr c_1 c_2}{\alpha^2} \left\{ \frac{1}{2 \alpha^2} - \frac{h^2}{12} - \frac{1}{h \alpha^3} \right\} + \frac{Ec_1^2}{\alpha^2} \left\{ \frac{1}{8 \alpha^2} - \frac{1}{8 h \alpha^3} \right\} \quad (22)$$

Heat Transfer Rate(Nusselt Number):

On the bottom:

$$\frac{d\theta}{dy} \Big|_{y=0} = \frac{1}{h} + \frac{Pr c_1 c_2}{\alpha^2} \left[\frac{-1}{\alpha^2 h} - \frac{h}{2} + \frac{1}{\alpha} \right] + \frac{Ec_1^2}{\alpha^2} \left[\frac{-1}{4 \alpha^2 h} + \frac{1}{2 \alpha} \right] \quad (23)$$

On the top:

$$\left. \frac{d\theta}{dy} \right|_{y=h} = \frac{1}{h} + \frac{Pr c_1 c_2}{\alpha^2} \left[\frac{-1}{\alpha^2 h} + \frac{h}{2} \right] + \frac{Ec_1^2}{\alpha^2} \left[\frac{-1}{4\alpha^2 h} \right] \quad (24)$$

2. Flow for shallow fluids. (i.e, for small h)

Retaining terms up to the $\mathcal{O}(h^2)$ and neglecting its higher powers we get

$$\text{Velocity: } v(y) = c_1 \left[\frac{(2hy - y^2)}{2} - \frac{\alpha^2}{24} (-4hy^3 + y^4) \right] \quad (25)$$

$$\text{Mean velocity: } \bar{v} = \frac{c_1 h^2}{3} \quad (26)$$

Temperature:

$$\begin{aligned} \theta(y) = & \frac{y}{h} + \frac{Pr c_1 c_2}{720} [(120hy^3 - 30y^4) - \alpha^2 (-6hy^5 + y^6)] + \\ & \frac{Ec_1^2}{180} [(60hy^3 - 90h^2y^2 - 15y^4) - \alpha^2 (15h^2y^4 - 12hy^5 + 2y^6)] \end{aligned} \quad (27)$$

Mean temperature:

$$\bar{\theta} = \frac{1}{h} \int_0^h \theta dy = \frac{1}{2} \quad (28)$$

Heat Transfer Rate(Nusselt Number):

On the bottom

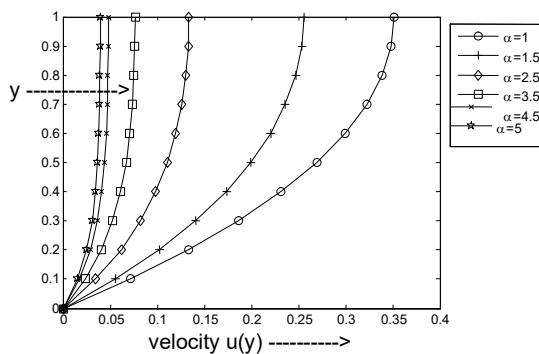
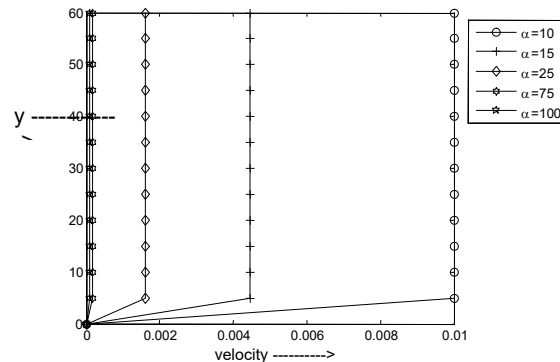
$$\left. \frac{d\theta}{dy} \right|_{y=0} = \frac{1}{h} \quad (29)$$

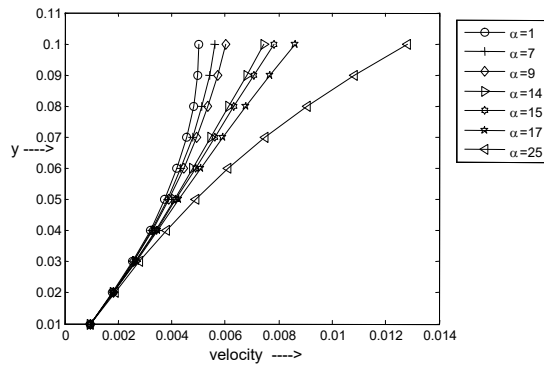
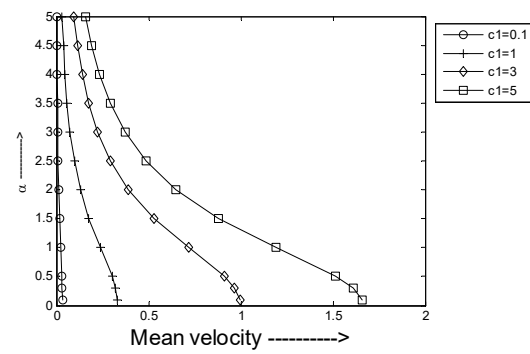
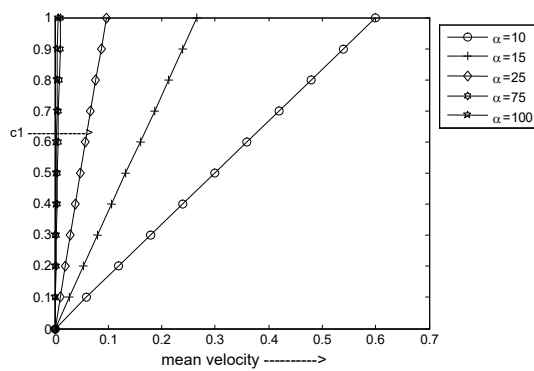
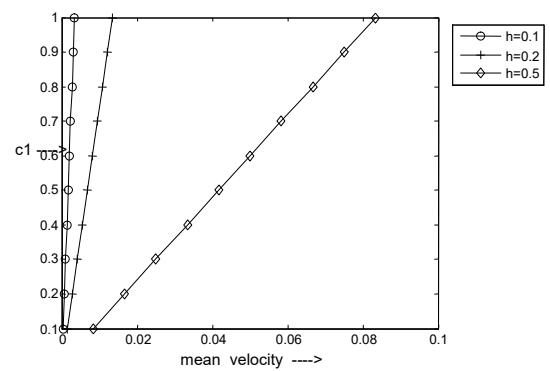
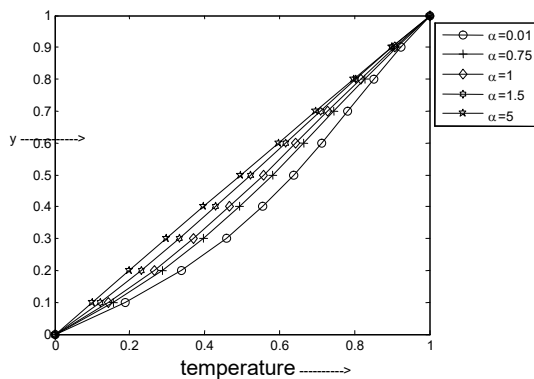
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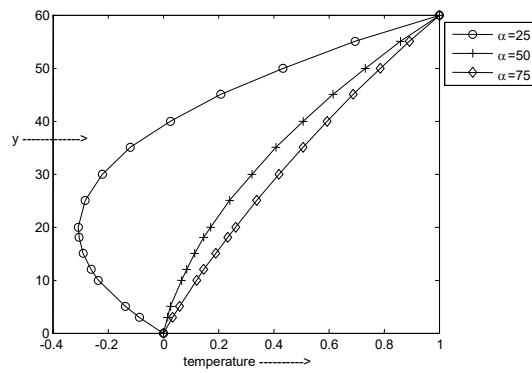
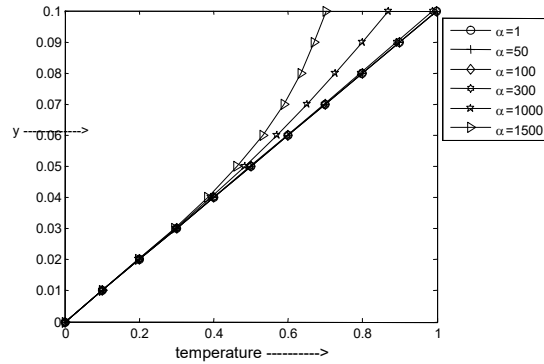
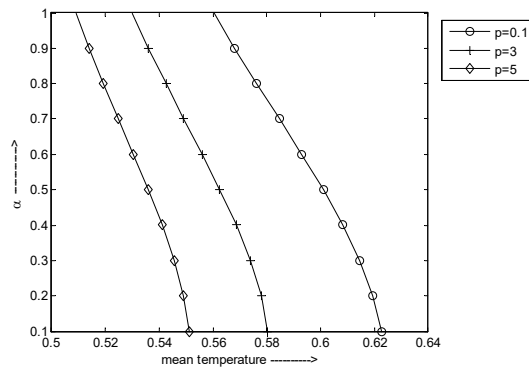
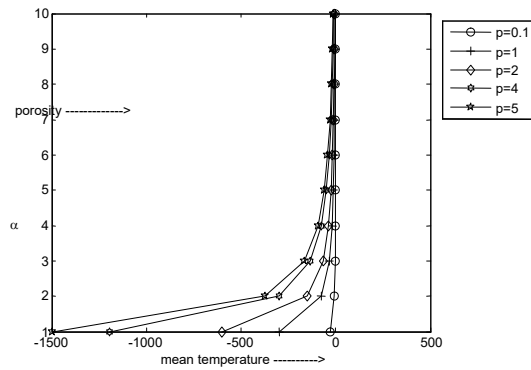
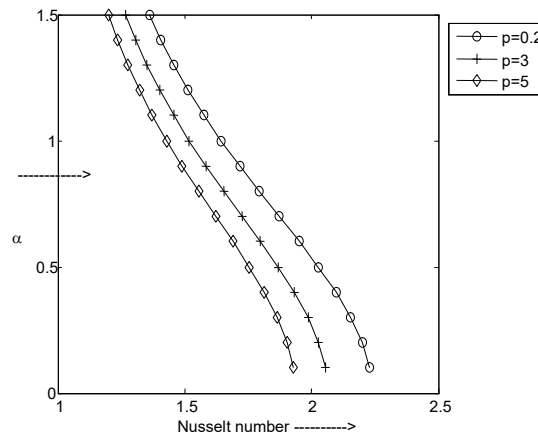
$$\left. \frac{d\theta}{dy} \right|_{y=h} = \frac{1}{h} \quad (30)$$

Conclusions:

1. It is noticed that the velocity profiles are more steep for large values of α that is the velocity of the fluid decreases with the increase in the value of α (fig 1). It can be observed from figure 1(a) thickness of the boundary layer decreases as the porosity parameter α increases .It can be observed from fig 1(b) the velocity of the flow region increases with the increase in the porosity parameter α .
2. It is evident from the fig 2 that for the increasing values of the pressure gradient c_1 the mean velocity increases and appears to be decreasing with the increase in the values of α . Figure 2(a) illustrates that the mean velocity decreases with the increase of the porosity parameter α Figure 2(b) illustrates that the mean velocity of the flow region increases with the increasing values of the pressure gradient c_1 and depth of the channel 'h'.
3. It is clearly illustrated in the fig 3 that the temperature profiles gradually decreases with the increase in the values of α . An increase in the porosity parameter α increases the temperature profile of the flow region. Fig.3(a). An increase in the porosity parameter α reduces the temperature of the flow region .Fig 3(b)
4. It is noticed that the mean temperature decreases as the prandtl number Pr increases along with the increase in the values of of the porosity parameter α (Fig .4). Figure 4(a) illustrates that the mean temperature decreases with increase of prandtl number Pr .
5. The rate of heat transfer (Nusselt Number) decreases with the increase in the values of α and the prandtl number 'Pr'.Fig.5. The rate of heat transfer on the bottom decreases with the increase in the values of the prandtl number Pr . Fig 5(a).
6. Fig.6 illustrates that the rate of heat transfer towards the free surface increases with the increase in the values of α as well as the prandtl number 'Pr'. Figure 6(a) illustrates that the Nusselt number increases on the free surface with the increase of the prandtl number Pr .


Fig 1 Velocity for $c_1=1$ and $h=1$

Fig. 1(a) velocity profile for large $h=60$


fig.1(b) velocity for small $h=1$

fig.2 mean velocity for $h=1$

Fig 2(a) mean velocity profile for large $h=60$

fig.2(b) mean velocity for small $h=1, 2, 3$

fig.3 Temperature distribution for $h=1, E=5, c1=1, c2=1, p=1$


fig.3(a) Temperature distribution for large $h=30, E=5, c_1=1, c_2=1, p=1$

fig.3(b) Temperature distribution for $p=1, h=1, E=5, c_1=1, c_2=1$

fig.4 Mean Temperature for $h=1, E=5, c_1=1, c_2=.5$

fig.4(a) mean temperature distribution for large $h=60, E=5, c_1=1, c_2=1$

fig.5 Nusselt number on the bottom for $h=1, E=5, c_1=1, c_2=.5$

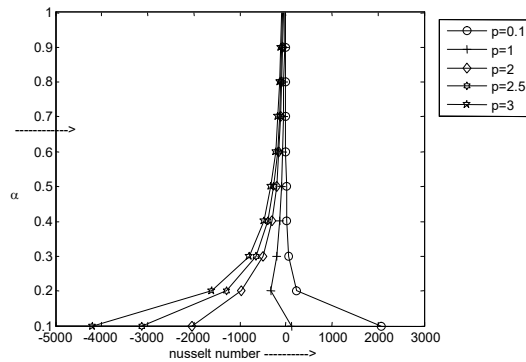


Fig 5(a) nusselt number for $h=60, E=5, c_1=1, c_2=1$

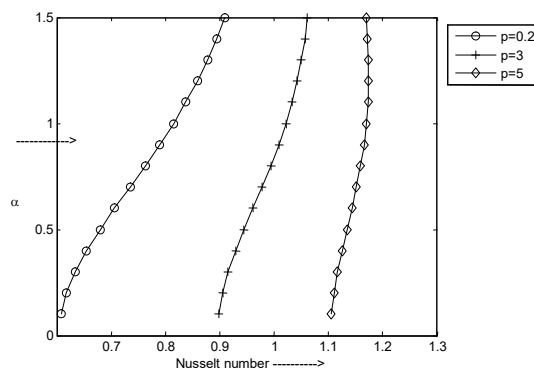


fig.6 Nusselt number on the top for $h=1, E=5, c_1=1, c_2=0.5$

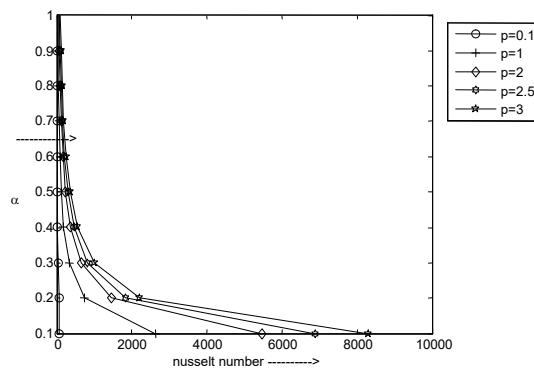


fig.6(a) nusselt number for $h=60, E=5, c_1=1, c_2=1$

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